

How to use asymptotics to derive a low-dimensional and mathematically well posed model of falling film flows.

Christian Ruyer-Quil¹, Khawla Msheik^{1,2}

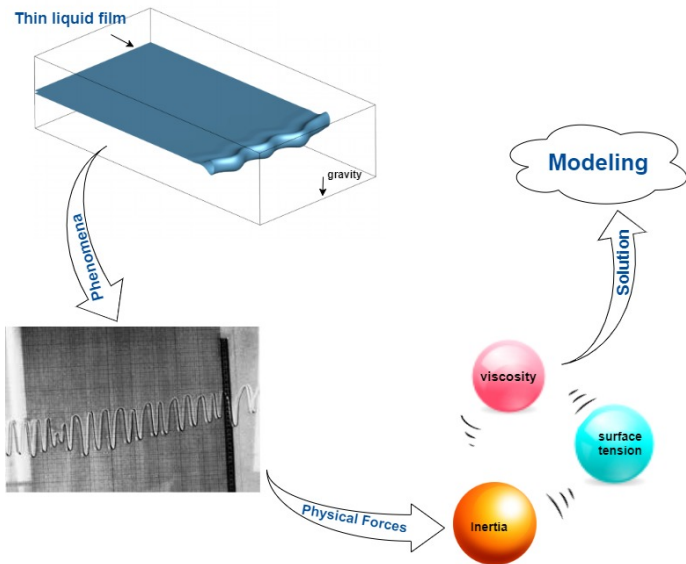
¹LOCIE, University Savoie Mont Blanc

²ICJ, University Claude Bernard (Lyon 1)

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Thin Films Between Physical Basis and Phenomena



Scaling For Thin Liquid Films

$$\left\{ \begin{array}{l} \nabla \cdot \mathbf{u} \\ \underbrace{\rho(\partial_t \mathbf{u} + \mathbf{u} \cdot \nabla \mathbf{u})}_{\text{Inertia}} \end{array} \right. = 0, \quad \underbrace{-\nabla p}_{\text{Pressure}} + \rho g \vec{e} + \underbrace{\mu \Delta \mathbf{u}}_{\text{Viscosity}} \cdot \xrightarrow{\text{Scaling}} \left\{ \begin{array}{l} \text{Reynold nb : } Re, \\ \text{Froude nb : } Fr, \\ \text{smallness parameter : } \epsilon \end{array} \right.$$

+B.C: Surface Tension

Ansatz: $Re = O(1)$

$$\epsilon Fr^2 \text{Inertia} = \epsilon (\text{Pressure} + \text{Surface Tension}) + \frac{Fr^2}{Re} (\text{Viscosity} + \text{Gravity})$$

- In Long wave limit: ϵ very small \implies Drag-gravity Regime
- What if ϵ is not too small \rightarrow What physical effect to count on, and what to ignore ?? \implies Drag-Inertia Regime

Weighted Residual Method [1]

- Start by choosing the velocity profile
 - ① At first order using Gauge condition

$$u = 3Ug_0 \text{ where } \underbrace{\int_0^h u = hU}_{\text{Gauge cnd}}$$

- ② Exact profile by adding the correction

$$u = 3Ug_0 + \epsilon \tilde{u} \iff \int_0^h \tilde{u} = 0$$

How to figure out \tilde{u} and other variables??

- Use Weighted residual method
 - ① From Mom EQ $\partial_{zz}u = 3U \partial_{zz}g_0 + \epsilon \partial_{zz}\tilde{u}$
 - ② Choose G such that by integration by parts

$$\int_0^h \partial_{zz}\tilde{u} \times G = B.C + \int_0^h \tilde{u} \underbrace{\partial_{zz}G}_{=cst} = C \int_0^h \tilde{u} = 0$$

- \tilde{u} eliminates from big orders of Mom EQ \rightarrow Solve obtained system for h and U

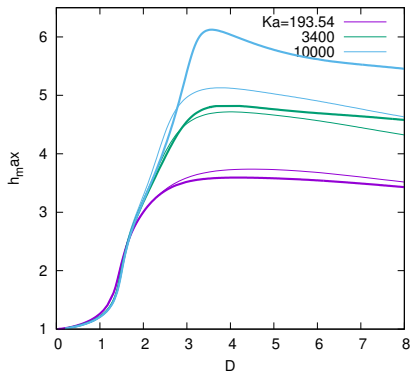
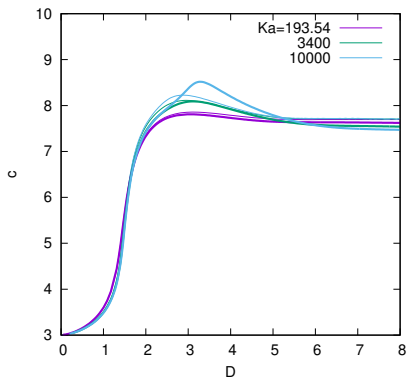
 " C. Ruyer-Quil, P. Manneville,
Improved modeling of flows down inclined planes, 2000

Pros of WRM

- Very good numerical results compared to Navier Stokes system results
- Better representation of Drag-inertia regimes where ϵ not very small

Cons

- No energy equation
- Lose hyperbolicity



" S. Chakraborty, P.-K. Nguyen, C. Ruyer-Quil and V. Bontozoglou,
Extreme solitary waves on falling liquid films, 2014

Propositions inspired by [1]

$$\epsilon \text{Inertia terms} = \text{Gravity} + \text{Viscosity} + \epsilon^2 \text{Dispersive terms}$$

- Viscosity terms give good eigenvalues \rightarrow Preserve them
- Change Inertia terms using Long wave expansion so that we
 - 1 Preserve the good representation Drag-inertia regime by WRM
 - 2 Obtain dissipative energy
 - 3 Obtain Linear stability



"[1] G. L. Richard, C. Ruyer-Quil and J. P. Vila,

A three-equation model for thin films down an inclined plane, 2016

First Approach

- **Comparison:**

Inertia terms from depth-integrating, i.e Shallow Water Model:

$$\partial_t(hU) + \partial_x\left(\int_0^h u^2\right) \quad \text{where} \quad \int_0^h u^2 = \int_0^h (U + u - U)^2 = hU^2 + O(\epsilon)$$

- **Idea:**

Better approximation of $\int_0^h (u - U)^2 \rightarrow$ Claim there exists ψ_1

$$\begin{aligned} \int_0^h (u - U)^2 &= \frac{h^3}{5} \left(U - 6\frac{s_1}{h}\right)^2 + O(\epsilon^2) && \text{...4 Eq Model by WRM} \\ &= \frac{h^3}{5} \psi_1^2 + O(\epsilon^2) \end{aligned}$$

- **Velocity profile**

$$\psi_1 = U - \frac{6s_1}{h} \implies u = F(U, \psi_1)$$

- **Procedure:**

Derive 3 equations on h , U , Ψ_1 using the residues

$$R_1 = \langle \tilde{u}, 1 \rangle = \int_0^h \tilde{u} dz = 0 \qquad R_2 = \langle \tilde{u}, g_0 \rangle = \int_0^h \tilde{u} g_0 dz = 0. \quad (1)$$

Transforming Inertia Terms: preserving consistency

- By WRM, we Solve above equations for $\partial_t U$ and $\partial_t \psi_1$

$$\underbrace{h \partial_t U + \dots}_{I_U} = \frac{1}{\epsilon Re} \left(\frac{14}{15} (\lambda h - \frac{3U}{h}) + \frac{21}{5} (\psi_1 - \frac{U}{h}) \right) - \frac{14}{15} \left(\frac{\cos \theta}{Fr^2} h \partial_x h - \frac{\kappa}{Fr^2} h \partial_x^3 h \right)$$

$$\underbrace{h \partial_t \psi_1 + \dots}_{I_{\psi_1}} = \frac{1}{\epsilon Re} \left(\frac{1}{3} (\lambda - \frac{3U}{h^2}) + \frac{21}{h} (\frac{U}{h} - \psi_1) \right) - \frac{1}{3} \left(\frac{\cos \theta}{Fr^2} \partial_x h - \frac{\kappa}{Fr^2} \partial_x^3 h \right)$$

- Using definition of ψ_1 and asymptotic expansions we prove

$$I_U \sim \partial_t(hU) + \underbrace{\partial_x(hU^2 + \frac{h^3 \psi_1^2}{5})}_{\partial_x(\int_0^h u^2)} + O(\epsilon^2)$$

$$I_{\psi_1} \sim \partial_t(h\psi_1) + \partial_x(hU\psi_1) - \frac{1}{7} \frac{\partial_x(h^4 \psi_1^3)}{h^2 \psi_1} + O(\epsilon)$$

Resulting System

$$\partial_t h + \partial_x(hU) = 0,$$

$$\begin{aligned} \partial_t(hU) + \partial_x(hU^2 + \frac{1}{5}h^3\psi_1^2) &= \frac{1}{\epsilon Re} \left(\frac{14}{15}(\lambda h - \frac{3U}{h}) + \frac{21}{5}(\psi_1 - \frac{U}{h}) \right) \\ &\quad - \frac{14}{15} \left(\frac{\cos\theta}{Fr^2} h \partial_x h - \frac{\kappa}{Fr^2} h \partial_x^3 h \right) + \frac{\epsilon}{Re} \mathcal{D}_1, \\ \partial_t(h\psi_1) + \partial_x(hU\psi_1) - \frac{1}{7} \frac{\partial_x(h^4\psi_1^3)}{h^2\psi_1} &= \frac{1}{\epsilon Re} \left(\frac{1}{3}(\lambda - \frac{3U}{h^2}) + \frac{21}{h}(\frac{U}{h} - \psi_1) \right) \\ &\quad - \frac{1}{3} \left(\frac{\cos\theta}{Fr^2} \partial_x h - \frac{\kappa}{Fr^2} \partial_x^3 h \right) + \frac{\epsilon}{Re} \mathcal{D}_2, \end{aligned} \tag{2}$$

- Term in violet approximation of $\int_0^h (u - U)^3$
- **Pros:** Dissipative energy

Numerical results of the Solitary wave test using AUTO

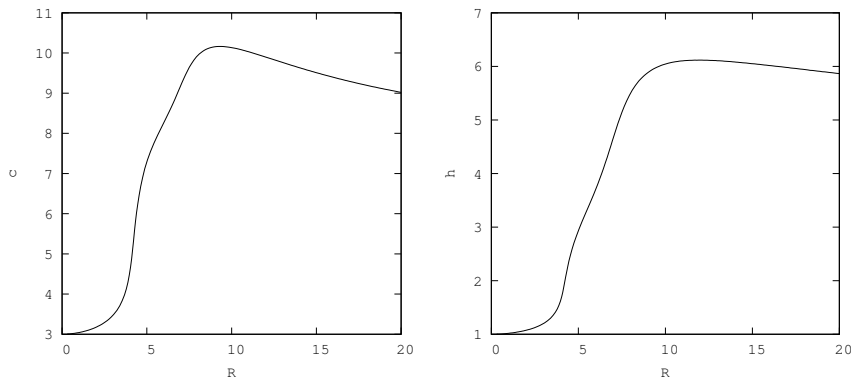


Figure 1: the height and velocity speed showing certain stability for sufficiently high Reynold number

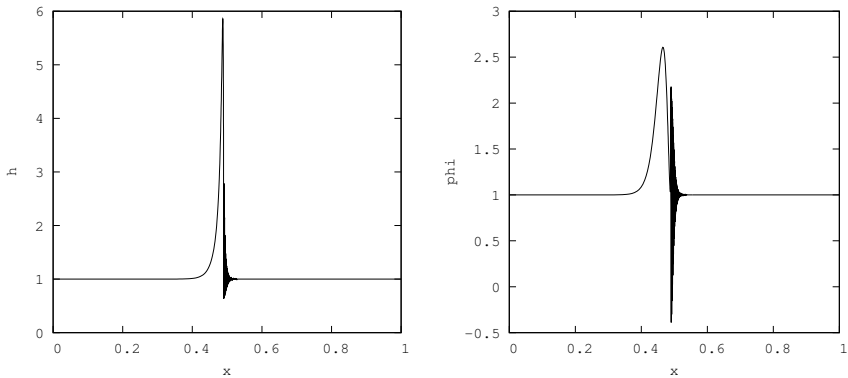


Figure 2: profiles of h and ψ_1 for $\text{Re}=20$, $\text{Ka}=3400$

- **One step further:** Claim there exists ψ_1 , ψ_2 and ψ_3

$$\begin{aligned} \int_0^h (u - U)^2 &= \frac{h^3}{5} \left(U - 6 \frac{s_1 + s_2}{h} \right)^2 + 4h^3 \left(s_1 - \frac{3}{2} s_2 \right)^2 + \frac{225}{13h} s_2^2 + O(\epsilon^2) \\ &= \frac{h^3}{5} \psi_1^2 + 4h^3 \psi_2^2 + \frac{225}{13} h^3 \psi_3^2 + O(\epsilon^2) \end{aligned}$$

- **Velocity profile**

$$u = F(U, \psi_1, \psi_2)$$

- **Procedure:** Derive 4 equations on h , U , $\Psi_{1,2}$, ($\Psi_3 = F(h, U, \Psi_1, \Psi_2)$) using

$$\begin{aligned} R_1 = \langle \tilde{u}, 1 \rangle &= \int_0^h \tilde{u} \, dz = 0 & R_2 = \langle \tilde{u}, g_0 \rangle &= \int_0^h \tilde{u} g_0 \, dz = 0 \\ R_3 = \langle \tilde{u}, g_1 \rangle &= \int_0^h \tilde{u} g_1 \, dz = 0. \end{aligned} \tag{3}$$

Goal: Reformulating inertia terms \rightarrow Dissipative Energy + linear stability

- First Eq: Easy

$$\partial_t(hU) + \partial_x(hU^2 + \frac{h^3\psi_1^2}{5} + 4h^3\psi_2^2) + O(\epsilon^2).$$

- Second Eq:

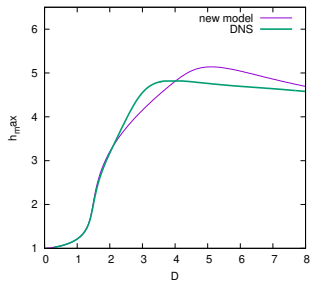
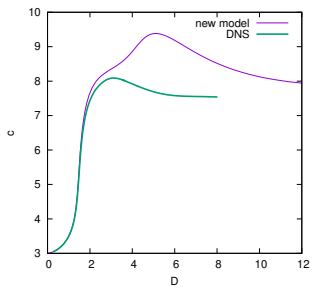
- 1 first approach as with ψ_1 with the term $-\frac{1}{7}\partial_x(h^3\psi_1^4)$:
failed to obtain the secondary fixed point

- 2 Second approach:

- 1 Preserve transport part for the sake of energy
- 2 Express different gradients that get canceled in mechanical energy equation

$$\begin{aligned} I_{\psi_1} &= \partial_t(h\psi_1) + \partial_x(hU\psi_1) + \frac{20}{h^2\psi_1} \left(\partial_x(A1h^3U\psi_1^2 + B1h^4\psi_1^3 + C1h^4\psi_1^2\psi_2) \right. \\ &\quad \left. - DDh^4\psi_2\psi_1 \partial_x\psi_1 - EEh^3\psi_2\psi_1^2 \partial_x h - FFh^3\psi_2\psi_1 \partial_x U - GGh^2\psi_2\psi_1 U \partial_x h \right) \\ &\quad + O(\epsilon) \\ I_{\psi_2} &= \partial_t(h\psi_2) + \partial_x(hU\psi_2) + \frac{1}{h^2\psi_2} \left(\partial_x(A2h^3U\psi_2^2 + B2h^4\psi_1\psi_2^2 + C2h^4\psi_2^3) \right. \\ &\quad \left. - DDh^4\psi_2\psi_1 \partial_x\psi_1 - EEh^3\psi_2\psi_1^2 \partial_x h - FFh^3\psi_2\psi_1 \partial_x U - GGh^2\psi_2\psi_1 U \partial_x h \right) \\ &\quad + O(\epsilon) \end{aligned} \tag{4}$$

Numerical Result



End of presentation



Thank You!